## Sheet:3

1- A generator is to be driven by a Pelton wheel with a head of 220 m and discharge rate of $145 \mathrm{~L} / \mathrm{s}$. The mean peripheral velocity of wheel is $14 \mathrm{~m} / \mathrm{s}$. If the outlet tip angle of the bucket is $160^{\circ}$, find out the power developed.

Using Euler's equation, work done per weight mass of water per sec

$$
=\left(C_{\mathrm{w} 1} U_{1}-C_{\mathrm{w} 2} U_{2}\right)
$$

Therefore
Work done $/ \mathrm{s}=\left(C_{\mathrm{w} 1} U_{1}+C_{\mathrm{w} 2} U_{2}\right) \mathrm{Nm} / \mathrm{s}$
From inlet velocity triangle

$$
C_{\mathrm{w} 1}=C_{1} \text { and } \frac{C_{1}^{2}}{2 g}=H
$$

Hence, $C_{1}=\sqrt{2 g H}=\sqrt{2 \times 9.81 \times 220}=65.7 \mathrm{~m} / \mathrm{s}$
Relative velocity at inlet is

$$
V_{1}=C_{1}-U_{1}=65.7-14=51.7 \mathrm{~m} / \mathrm{s}
$$

From outlet velocity triangle

$$
V_{1}=V_{2}=51.7 \mathrm{~m} / \mathrm{s} \text { (neglecting friction) }
$$

and $\cos \beta_{2}=\frac{U_{2}+C_{\mathrm{w} 2}}{V_{2}}$ or


$$
\cos (20)=\frac{14+C_{\mathrm{w} 2}}{51.7}
$$

Therefore

$$
C_{\mathrm{w} 2}=34.58 \mathrm{~m} / \mathrm{s}
$$

Hence, work done per unit mass of water per sec.

$$
=(65.7)(14)+(34.58)(14)=1403.92 \mathrm{Nm}
$$

Power developed $=\frac{(1403.92)(145)}{1000}=203.57 \mathrm{~kW}$

2- A Pelton wheel is supplied with $0.035 \mathrm{~m}^{3} / \mathrm{s}$ of water under a head of 92 m . The wheel rotates at 725 rpm and the velocity coefficient of the nozzle is 0.95 . The efficiency of the wheel is $82 \%$ and the ratio of bucket speed to jet speed is 0.45 . Determine the following: 1 . Speed of the wheel 2 . Wheel to jet diameter ratio 3. Dimensionless power specific speed of the wheel.

3- A generator is driven by a small, single-jet Pelton turbine designed to have a power specific speed $\Omega_{\mathrm{SP}}=0.20$. The effective head at nozzle inlet is 120 m and the nozzle velocity coefficient is 0.985 . The runner rotates at $880 \mathrm{rev} / \mathrm{min}$, the turbine overall efficiency is $88 \%$ and the mechanical efficiency is $96 \%$. If the blade speed to jet speed ratio, $v=0.47$, determine (i) the shaft power output of the turbine; (ii) the volume flow rate; (iii) the ratio of the wheel diameter to jet diameter..

Solution. (1) With eqn (9.1) the power specific speed is $\Omega_{s}=\frac{\Omega \sqrt{P / p^{p}}}{\left(g H_{e}\right)^{\frac{3}{4}}}$
where $\Omega=\frac{\pi g}{30} N=92.15 \mathrm{rad} / \mathrm{s}$. Hence,

$$
P=p\left[\frac{\Omega_{\mathrm{o}}}{\Omega}\left(g H_{t}\right)^{314}\right]^{2}=10^{3}\left[\frac{0.2}{92.15}(9.81 \times 120)^{1.25}\right]^{2}=224,000 \mathrm{~W}
$$

$\therefore P=224 \mathrm{~kW}$
(2) The overall efficiency is given by $z_{B}=P /\left\{\left\{g Q Q H_{e}\right\}\right.$

$$
\text { hence } Q=\frac{P}{\mu g \eta_{0} H_{e}}=\frac{224 \times 10^{3}}{10^{3} \times 9.81 \times 0.88 \times 120}=0.2162 \mathrm{~m}^{3 / \mathrm{s}}
$$

(3) The jet velocity is given by:

$$
c_{1}=K_{N} \sqrt{2 g H_{c}}=0.985 \sqrt{2 \times 9.81 \times 120}=47.79 \mathrm{~m} / \mathrm{s}
$$

The blade speed is: $U=\operatorname{s.r}^{\circ} C_{1}=0.47 \times 47.79=22.46 \mathrm{~m} / \mathrm{s}$

$$
\begin{gathered}
D=\frac{2 U}{52}=\frac{2 \times 22.46}{92.15}=0.4875 \mathrm{~m} \\
\text { As } Q=\frac{5 \pi}{4} d^{2} c_{1} \text { then } d=\sqrt{\frac{4 Q}{\pi c_{1}}}=\sqrt{\frac{4 \times 0.2162}{\pi \times 47.79}}=0.07589 \\
\therefore \frac{D}{d}=6.423
\end{gathered}
$$

4- A multi-jet Pelton turbine with a wheel 1.47 m diameter, operates under an effective head of 200 m at nozzle inlet and uses $4 \mathrm{~m}^{3} / \mathrm{s}$ of water. Tests have proved that the wheel efficiency is $88 \%$ and the velocity coefficient of each nozzle is 0.99 . Assuming that the turbine operates at a blade speed to jet speed ratio of 0.47 , determine (i) the wheel rotational speed; (ii) the power output and the power specific speed; (iii) the bucket friction coefficient given that the relative flow is deflected $165^{\circ}$; (iv) the required number of nozzles if the ratio of the jet diameter to mean diameter of the wheel is limited to a maximum value of 0.113 .

5- A Francis turbine operates at its maximum efficiency point at $\eta_{0}=0.94$, corresponding to a power specific speed of 0.9 rad . The effective head across the turbine is 160 m and the speed required for electrical generation is $750 \mathrm{rev} / \mathrm{min}$. The runner tip speed is 0.7 times the spouting velocity, the absolute flow angle at runner entry is 72deg from the radial direction and the absolute flow at runner exit is without swirl. Assuming there are no losses in the guide vanes and the mechanical efficiency is $100 \%$, determine (i) the turbine power and the volume flow rate; (ii) the runner diameter; (iii) the magnitude of the tangential component of the absolute velocity at runner inlet; (iv) the axial length of the runner vanes at inlet..

6- The power specific speed of a 4MW Francis turbine is 0.8 , and the hydraulic efficiency can be assumed to be $90 \%$. The head of water supplied to the turbine is 100 m . The runner vanes are radial at inlet and their internal diameter is three quarters of the external diameter. The meridional velocities at runner inlet and outlet are equal to 25 and $30 \%$, respectively, of the spouting velocity. Determine (i) the rotational speed and diameter of the runner; (ii) the flow angles at outlet from the guide vanes and at runner exit; (iii) the widths of the runner at inlet and at exit. Blade thickness effects can be neglected.

7- A propeller turbine develops $12,000 \mathrm{hp}$, and rotates at 145 rpm under a head of 20 m . The outer and hub diameters are 4 m and 1.75 m , respectively. Calculate the inlet and outlet blade angles measured at mean radius if overall and hydraulic efficiencies are $85 \%$ and $93 \%$, respectively

